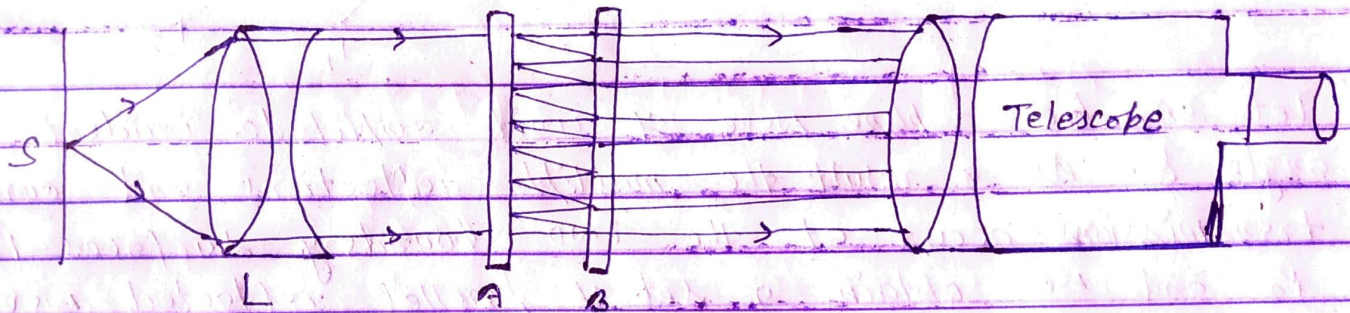


## Fabry Perot Interferometer : →

In this interferometer the sharp Haidinger fringes are produced by means of multiple reflections from two partially silvered plates separated from each other.

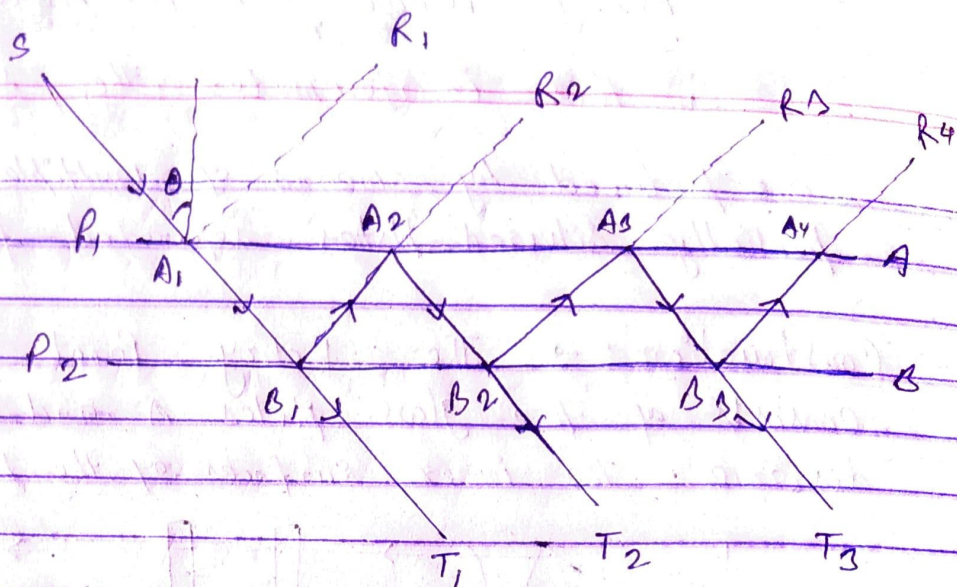
→ Construction : → The Fabry Perot interferometer essentially consists of two glass plates A and B separated by a distance. The inner surfaces of the plates are coated with



a thin film of aluminium which reflects about 75% of the incident light. The plate B facing the observer is fixed and is provided with screws with which the reflecting surface of B can be made parallel to that of A. The plate A is mounted on a carriage which can be moved in a direction  $\perp$  to the reflecting surfaces by means of an accurate screw so that the thickness of air film between the coated surfaces of the plates A and B can be varied. Light from monochromatic extended source rendered parallel by collimating lens L, suffers multiple reflections in the air film between plates A and B. The transmitted light interferes and circular fringes of equal inclination are formed at the focal plane of the objective of the telescope.

→ Theory of intensity distribution →

In fig  $P_1$  and  $P_2$  represent reflecting surfaces of the two plates A and B. Light from a monochromatic extended source is incident on the plates at all angles.



Let  $SA_1$  be a plane wave of unit amplitude incident at an angle  $\theta$ . As a result the multiple reflections and consequent transmissions occur at the two boundary surfaces  $P_1$  and  $P_2$  and we obtain a set of parallel reflected waves  $A, R_1, A_2, R_2, A_3, R_3, \dots$  etc. and a set of parallel infinite transmitted beams  $B, T_1, B_2, T_2, B_3, T_3, \dots$  etc. Let  $R$  and  $T$  be the fractions of intensity which are reflected and transmitted, i.e. the reflection and transmission coefficients. Obviously the fractions of amplitudes reflected and transmitted are  $\sqrt{R}$  and  $\sqrt{T}$ . As the amplitude of the incident wave is unity, the amplitude of wave  $A_1, B_1$  is  $\sqrt{T}$  and the amplitude of wave  $B_1, T_1$  is  $(\sqrt{T} \times \sqrt{T}) = T$ . The amplitude of wave  $B_1, A_2$  is  $\sqrt{RT}$  and the amplitude of the wave  $A_2, B_2$  is  $(\sqrt{R} \times \sqrt{RT}) = R\sqrt{T}$  and the amplitude of the wave  $B_2, T_2$  is  $RT$ . Similarly the amplitudes of waves  $B_3, T_3, B_4, T_4$  etc. are  $R^2T, R^3T, \dots$  etc. Thus the amplitudes along  $A, T_1, B_2, T_2, A_3, T_3, B_4, T_4$  etc. are  $T, RT, R^2T, \dots$  etc.

As all the transmitted waves  $B_1, T_1, B_2, T_2, B_3, T_3$  have been obtained from the same incident wave, they are capable of producing interference pattern.

Neglecting any phase change due to reflection from the silvered surfaces, there is a const. phase difference

between any two consecutive transmitted beams due to path difference  $2\mu t \cos \theta$ .

$\therefore$  Phase diff. between two consecutive transmitted beams.

$$\delta = \frac{2\pi}{\lambda} \times 2\mu t \cos \theta$$

$$= \frac{2\pi}{\lambda} \cdot 2t \cos \theta \quad \text{--- --- --- } \textcircled{1} \quad (\because \text{for air film } \mu=1)$$

Let the incident vibration be represented by

$$y' = 1 \cdot \sin \omega t$$

so that, the transmitted waves along  $B_1T_1, B_2T_2, B_3T_3, \dots$  etc. at the point of interference will be represented by

$$y_1 = T \sin \omega t, \quad y_2 = TR \sin(\omega t - \delta)$$

$$y_3 = TR^2 \sin(\omega t - 2\delta), \quad y_4 = TR^3 \sin(\omega t - 3\delta), \dots \text{ etc.}$$

If  $A$  is the amplitude of the resultant vibration and  $\phi$  its phase difference, then

$$y = A \sin(\omega t - \phi)$$

By the principle of superposition, we have

$$y = y_1 + y_2 + y_3 + \dots$$

$$\therefore A \sin(\omega t - \phi) = T \sin \omega t + RT \sin(\omega t - \delta) + R^2 T \sin(\omega t - 2\delta) + \dots$$

Expanding the sine terms and equating the coeffs. of  $\sin \omega t$  and  $\cos \omega t$ , we get

$$A \cos \phi = T + TR \cos \delta + TR^2 \cos 2\delta + \dots \quad \textcircled{2}$$

$$A \sin \phi = TR \sin \delta + TR^2 \sin 2\delta + \dots \quad \textcircled{1}$$

As  $A$  is complex quantity, the resultant intensity is given by

$$I = A^2 = (A \cos \phi + iA \sin \phi)(A \cos \phi - iA \sin \phi) \quad \text{--- (4)}$$

where  $i = \sqrt{-1}$

But from (2) & (3), we have

$$A \cos \phi + iA \sin \phi = T (1 + R e^{i\delta} + R^2 e^{2i\delta} + \dots)$$

$$= \frac{T}{1 - R e^{i\delta}}$$

$$\text{and } A \cos \phi - iA \sin \phi = T (1 + R e^{-i\delta} + R^2 e^{-2i\delta} + \dots)$$

$$= \frac{T}{1 - R e^{-i\delta}}$$

$\therefore$  Resultant intensity at the point of interference due to transmitted vibrations is

$$I = A^2 = \frac{T}{(1 - R e^{i\delta})} \times \frac{T}{(1 - R e^{-i\delta})}$$

$$= \frac{T^2}{1 + R^2 - 2R \cos \delta} = \frac{T^2}{(1-R)^2 + 2R - 2R \cos \delta}$$

$$= \frac{T^2}{(1-R)^2 + 2R(1 - \cos \delta)} = \frac{T^2}{(1-R)^2 + 4R \sin^2 \frac{\delta}{2}}$$

$$= \frac{T^2}{(1-R)^2 + 4R \sin^2 \frac{\delta}{2}}$$

$$= \frac{T^2}{(1-R)^2 \left[ 1 + \frac{4R}{(1-R)^2} \sin^2 \frac{\delta}{2} \right]}$$

(5)

Thus the resultant intensity varies with  $R$  &  $\delta$ .

→ Condition for maxima and minima: →

for maximum intensity  $\sin^2 \frac{\delta}{2} = 0$ , i.e.  $\frac{\delta}{2} = n\pi$

∴  $\delta = 2n\pi = 0, 1, 2, 3, \dots$  etc.

The maximum intensity will be  $I_{\max} = \frac{T^2}{(1-R)^2}$  --- (6)

for minimum intensity,

$$\sin^2 \frac{\delta}{2} = 1$$

$$\text{i.e. } \frac{\delta}{2} = (2n+1) \frac{\pi}{2}$$

$$\text{∴ } \delta = (2n+1) \pi = (2n+1) \frac{\pi}{2}$$

And the minimum intensity will be

$$I_{\min} = \frac{T^2}{(1-R)^2} \cdot \frac{1}{\left[1 + \frac{4R}{(1-R)^2}\right]}$$

$$= \frac{T^2}{(1+R)^2}$$

when there is no absorption for light on the plates,

$$T+R = 1$$

$$\text{∴ } T = 1 - R$$

This gives,  $I_{\max} = 1$

$$\text{and } I_{\min} = \frac{(1-R)^2}{(1+R)^2}$$

(8)

Using eqn (6), eqn (5) can be written as

$$I = I_{\max} \frac{1}{1 + F \sin^2 \frac{\delta}{2}} \quad (9)$$

$$\text{Where } F = \frac{4R}{(1-R)^2} \quad (10)$$

and is called the coefficient of fineness or coefficient of sharpness.

$$\text{From eqn (9)} \quad \frac{I}{I_{\max}} = \frac{1}{1 + F \sin^2 \frac{\delta}{2}} \quad (11)$$

The condition for maxima and minima in terms of path difference are

$$2t \cos \theta = n \lambda \quad (\text{maxima})$$

$$2t \cos \theta = (2n-1) \frac{\lambda}{2} \quad (\text{minima})$$

As 't' is constant, for a particular value of n and  $\lambda$ ,  $\theta$  must be constt. The locus of all points having same value of  $\theta$  is a circle. Therefore the fringes are circular in shape.

— \* —

Dr. Sanjay - Kumar  
Dept. of Physics  
S.O.S. College Jabalpur